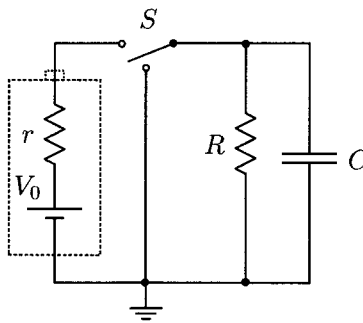
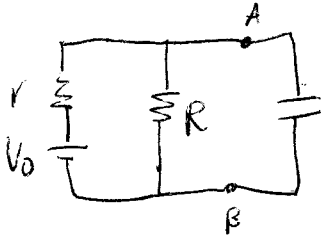


Free Response: Write out complete answers to the following questions. Show your work.

- (15pts) 1. The circuit below has a battery, a switch S , and a resistor R in parallel with capacitor C . The battery is modelled as a voltage source V_0 in series with resistor r which represents the internal resistance of the battery.

w/ switch in up position

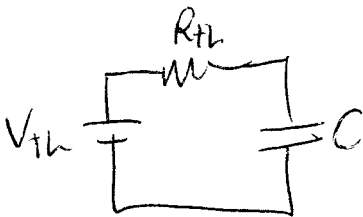


- (a) Suppose that the switch S is initially in the down position for a long time and then, at time $t = 0$, it is moved to the up position. If $V_0 = 9.0 \text{ V}$, $r = 1.5 \Omega$, $R = 16 \text{ k}\Omega$, and $C = 22 \mu\text{F}$, how long does it take the capacitor acquire a charge of 0.11 mC ? (5 marks)

replace everything to left of terminals A & B w/ Thevenin equiv \rightarrow voltage divider

$$V_{th} = V_0 \frac{R}{r+R} (\approx V_0)$$

$$R_{th} = \frac{rR}{r+R} (\approx r)$$



$$V_C(t) = V_{th} (1 - e^{-t/\tau}) \quad \tau = R_{th}C$$

$$\therefore \frac{V_C(t)}{V_{th}} = 1 - e^{-t/\tau} \quad -\frac{t}{\tau} = \ln\left(1 - \frac{V_C(t)}{V_{th}}\right)$$

$$t = -\tau \ln\left(1 - \frac{V_C(t)}{V_{th}}\right)$$

$$C = \frac{q}{V_C} \quad \therefore V_C(t) = \frac{q(t)}{C}$$

$$\therefore t = -\tau \ln\left(1 - \frac{q/C}{V_{th}}\right)$$

$$\tau = R_{th}C = \frac{rR}{r+R}C = 33.0 \mu\text{s}$$

$$V_{th} = 9.00 \text{ V}$$

$$\therefore t = 26.8 \mu\text{s}$$

(b) Now suppose that the switch has been in the up position for an unknown amount of time. Then, at $t = 0$, it is moved into the down position to discharge the capacitor. The voltage across the capacitor V_c and its uncertainty are measured as a function of time as shown in the table below. Also shown in the table are the values of $\ln V_c$. Complete the table by entering the error in $\ln V_c$ in the final column of the table. Clearly explain how these values are obtained. (5 marks)

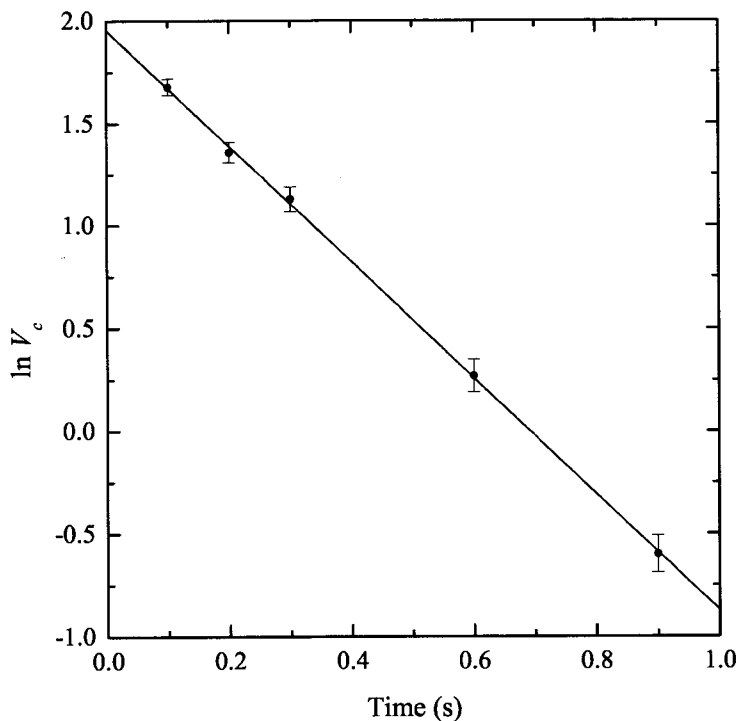
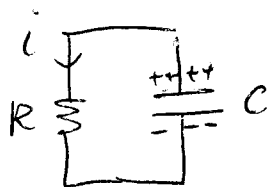
t (s)	V_c (V)	ΔV_c (V)	$\ln V_c$	$\Delta(\ln V_c)$
0.1	5.4	0.2	1.68	0.04
0.2	3.9	0.2	1.36	0.05
0.3	3.1	0.2	1.13	0.06
0.6	1.31	0.1	0.27	0.08
0.9	0.55	0.05	-0.60	0.09

$$\Delta(\ln V_c) = \left| \frac{\partial \ln V_c}{\partial V_c} \Delta V_c \right|$$

$$\therefore \Delta(\ln V_c) = \frac{\Delta V_c}{V_c}$$

(c) The $\ln V_c$ versus t data from the table are plotted below and fit to a straight line. The equation of the best-fit line is $y = mx + b$ with $m = -2.83 \pm 0.05 \text{ s}^{-1}$ and $b = 1.95 \pm 0.02$. Use this information to determine the initial voltage across the capacitor at $t = 0$ and its uncertainty $[V_c(0) \pm \Delta V_c(0)]$ and the time constant of the decay and its uncertainty $[\tau \pm \Delta\tau]$. Does the experimentally determined value of τ agree with the expected value? (5 marks)

w/ switch in down position circuit becomes



For discharging cap $V_c(t) = V_c(0) e^{-\frac{t}{\tau}}$ where $\tau = RC$
 $= (16 \text{ k}\Omega)(22 \mu\text{F}) = 0.352 \text{ s}$

eqn of straight line

w/ $b = \ln V_c(0)$ $m = -\frac{1}{\tau}$

$\therefore V_c(0) = e^b$
 $\Delta V_c(0) = \left| \frac{\partial e^b}{\partial b} \Delta b \right| = e^b \Delta b$

$\therefore V_c(0) = 7.03 \pm 0.14 \text{ V}$

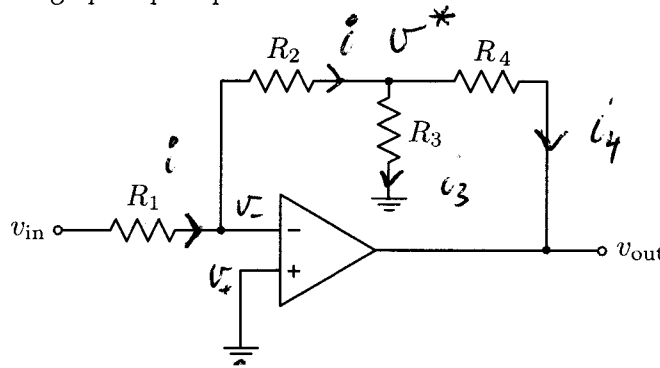
$\tau = -\frac{1}{m}$
 $\Delta\tau = \left| \frac{\partial(-\frac{1}{m})}{\partial m} \Delta m \right| = \left| \frac{\Delta m}{m^2} \right|$

$\therefore \tau = 0.353 \pm 0.006 \text{ s}$

experimental value agrees w expected value.

0pts

(10pts) 2. Consider the following op-amp amplifier circuit:



(a) Find an expression for the gain ($G = v_{out}/v_{in}$) of the amplifier in terms of R_1 , R_2 , R_3 , and R_4 . (7 marks)

op amp golden rules: $i_- = i_+ = 0$
 $v_+ = v_- = 0$

$$v_{in} - iR_1 = v_- = 0 \quad \Rightarrow \quad i = \frac{v_{in}}{R_1}$$

$$v_- - iR_2 = v^*$$

$$\therefore v^* = -iR_2 = -v_{in} \frac{R_2}{R_1}$$

$$v^* - i_3 R_3 = 0$$

$$\therefore i_3 = \frac{v^*}{R_3} = -v_{in} \frac{R_2}{R_1 R_3}$$

$$v^* - i_4 R_4 = v_{out}$$

$$\therefore i_4 = \frac{v^* - v_{out}}{R_4} = -v_{in} \frac{R_2}{R_1 R_4} - \frac{v_{out}}{R_4}$$

By junction rule

$$i = i_3 + i_4$$

$$\therefore \frac{v_{in}}{R_1} = -v_{in} \frac{R_2}{R_1 R_3} - \frac{v_{out}}{R_4}$$

solve for v_{out}

$$\frac{v_{out}}{R_4} = -v_{in} \left[\frac{R_2}{R_1 R_3} + \frac{R_2}{R_1 R_4} + \frac{1}{R_1} \right]$$

$$\therefore v_{out} = -v_{in} \left[\frac{R_2 R_4}{R_1 R_3} + \frac{R_2}{R_1} + \frac{R_4}{R_1} \right]$$

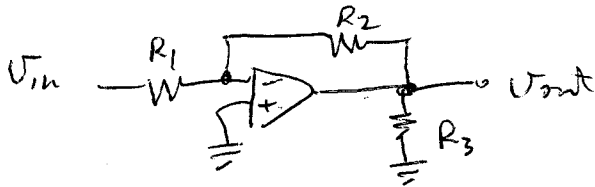
$$= -v_{in} \left[\frac{R_2 R_4 + R_2 R_3 + R_3 R_4}{R_1 R_3} \right]$$

(b) What does the gain become if $R_4 = 0$? Does this result agree with what you would expect? Explain. (2 marks)

$$\text{If } R_4 = 0 \quad V_{\text{out}} = - \frac{V_{\text{in}}}{R_1 R_3} [R_2 R_3] = -V_{\text{in}} \frac{R_2}{R_1}$$

This is the inverting amplifier result.

w/ $R_4 = 0$ circuit becomes



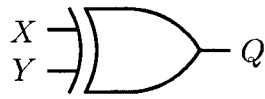
Here R_3 is irrelevant
& have inverting amp circuit.

(c) What is the gain of the amplifier if $R_1 = R_3 = 1 \text{ k}\Omega$ and $R_2 = R_4 = 100 \text{ k}\Omega$? (1 mark)

$$\frac{V_{\text{out}}}{V_{\text{in}}} = - \frac{1}{(1 \text{ k}\Omega)(1 \text{ k}\Omega)} \left[(100 \text{ k}\Omega)(100 \text{ k}\Omega) + (100 \text{ k}\Omega)(1 \text{ k}\Omega) + (1 \text{ k}\Omega)(100 \text{ k}\Omega) \right]$$

$$= -10^4 + 2 \cdot 10^2 = \boxed{-10,200}$$

(10pts) 3. The XOR gate and its truth table are shown below.

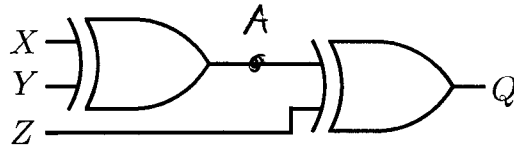


X	Y	$Q = X \oplus Y$
0	0	0
0	1	1
1	0	1
1	1	0

The XOR gate can be thought of as a two-input "parity" checker. If an odd number of inputs are high, then the output is high. Alternatively, if zero or an even number of the inputs are high, then the output is low.

(a) Confirm that the circuit below acts as a three-input parity checker. Do this by writing out the complete truth table for this circuit and confirming that it works as required. (4 marks)

*3 inputs,
2³ possible input comb's
8*



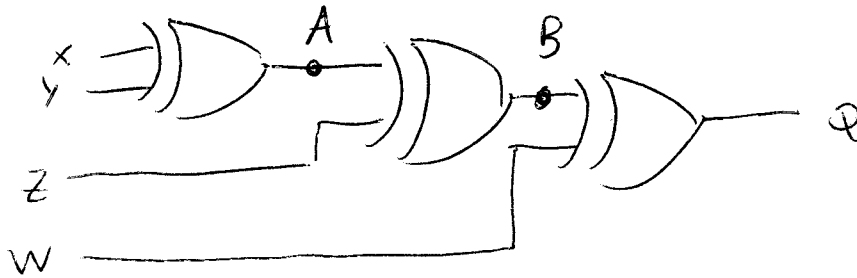
	X	Y	Z	$A = X \oplus Y$	$Q = A \oplus Z$
zero	0	0	0	0	0 ✓
odd	0	0	1	0	1 ✓
odd	0	1	0	1	1 ✓
even	0	1	1	1	0 ✓
odd	1	0	0	1	1 ✓
even	1	0	1	1	0 ✓
even	1	1	0	0	0 ✓
odd	1	1	1	0	1 ✓

works as expected

→ 3 input parity checker

(6) Design a four-input parity checking circuit. Construct the complete truth table to confirm that the circuit that you designed works as required. (6 marks)

Try



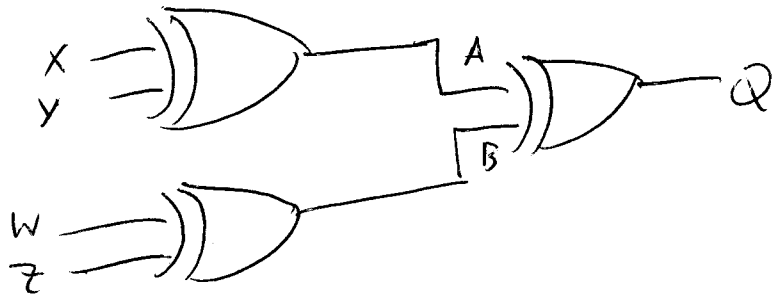
$2^4 \rightarrow 16$
possible input
combos

X	Y	Z	W	$A = X \oplus Y$	$B = A \oplus Z$	$Q = B \oplus W$	even or odd?
0	0	0	0	0	0	0	zero ✓
0	0	0	1	0	0	1	odd ✓
0	0	1	0	0	1	1	odd ✓
0	0	1	1	0	1	0	even ✓
0	1	0	0	1	1	1	odd ✓
0	1	0	1	1	1	0	even ✓
0	1	1	0	1	0	0	even ✓
0	1	1	1	1	0	1	odd ✓
1	0	0	0	1	1	1	odd ✓
1	0	0	1	1	1	0	even ✓
1	0	1	0	1	0	0	even ✓
1	0	1	1	1	0	1	odd ✓
1	1	0	0	0	0	0	even ✓
1	1	0	1	0	0	1	odd ✓
1	1	1	0	0	1	1	odd ✓
1	1	1	1	0	1	0	even ✓

works
as required
4-input
parity
checker.

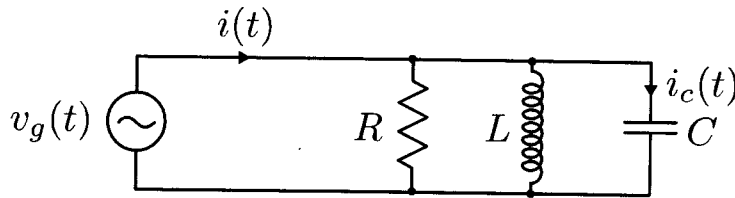
0pts

Note that the circuit below also works



$X Y W Z$	$A = X \oplus Y$	$B = W \oplus Z$	$Q = A \oplus B$	even or odd
0000	0	0	0	zero
0001	0	1	1	odd
0010	0	1	1	odd
0011	0	0	0	even
0100	1	0	1	odd
0101	1	1	0	even
0110	1	1	0	even
0111	1	0	1	odd
1000	1	0	1	odd
1001	1	1	0	even
1010	1	1	0	even
1011	1	0	1	odd
1100	0	0	0	even
1101	0	1	1	odd
1110	0	1	1	odd
1111	0	0	0	even

- (20pts) 4. Consider the parallel LRC circuit shown below. The function generator supplies $v_g(t) = V_0 \sin \omega t$ to the circuit.



(a) Find expressions for the amplitude I_0 and phase ϕ of the current $i(t) = I_0 \sin(\omega t + \phi)$ shown in the figure above. Give your expressions in terms of R, L, C, ω , and V_0 . (8 marks)

$$I_0 = \frac{V_0}{|Z|} \quad \tan \phi = \frac{\text{Im}[Z^*]}{\text{Re}[Z]}$$

$$Z = R \parallel Z_L \parallel Z_C$$

$$\frac{1}{Z} = \frac{1}{R} + \frac{1}{j\omega L} + j\omega C = \frac{1}{R} + j\left(\omega C - \frac{1}{\omega L}\right)$$

$$\therefore \frac{1}{|Z|^2} = \left[\frac{1}{R} + j\left(\omega C - \frac{1}{\omega L}\right) \right] \left[\frac{1}{R} - j\left(\omega C - \frac{1}{\omega L}\right) \right] = \frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2$$

$$\therefore \frac{1}{|Z|} = \sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}$$

$$\therefore I_0 = V_0 \sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}$$

$$Z = \frac{1}{\frac{1}{R} + j\left(\omega C - \frac{1}{\omega L}\right)} \cdot \frac{\frac{1}{R} - j\left(\omega C - \frac{1}{\omega L}\right)}{\frac{1}{R} - j\left(\omega C - \frac{1}{\omega L}\right)} = \frac{\frac{1}{R} - j\left(\omega C - \frac{1}{\omega L}\right)}{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}$$

$$\therefore Z^* = \frac{\frac{1}{R} + j\left(\omega C - \frac{1}{\omega L}\right)}{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}$$

$$\therefore \tan \phi = \frac{+\left(\omega C - \frac{1}{\omega L}\right)}{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2} \cdot \frac{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}{\frac{1}{R}}$$

$$\therefore \tan \phi = R \left(\frac{-1}{\omega L} + \omega C \right)$$

(b) For values of $\omega \gg 1/\sqrt{LC}$, show that I_0 can be approximated as $I_0 \approx A\omega^n$. Determine A and n . (2 marks)

for $\omega \rightarrow \infty$ $I_0 \approx V_0 \sqrt{\frac{1}{R^2} + (\omega C)^2} \approx V_0 C \omega$
 $\therefore A = V_0 C$
 $n = 1$

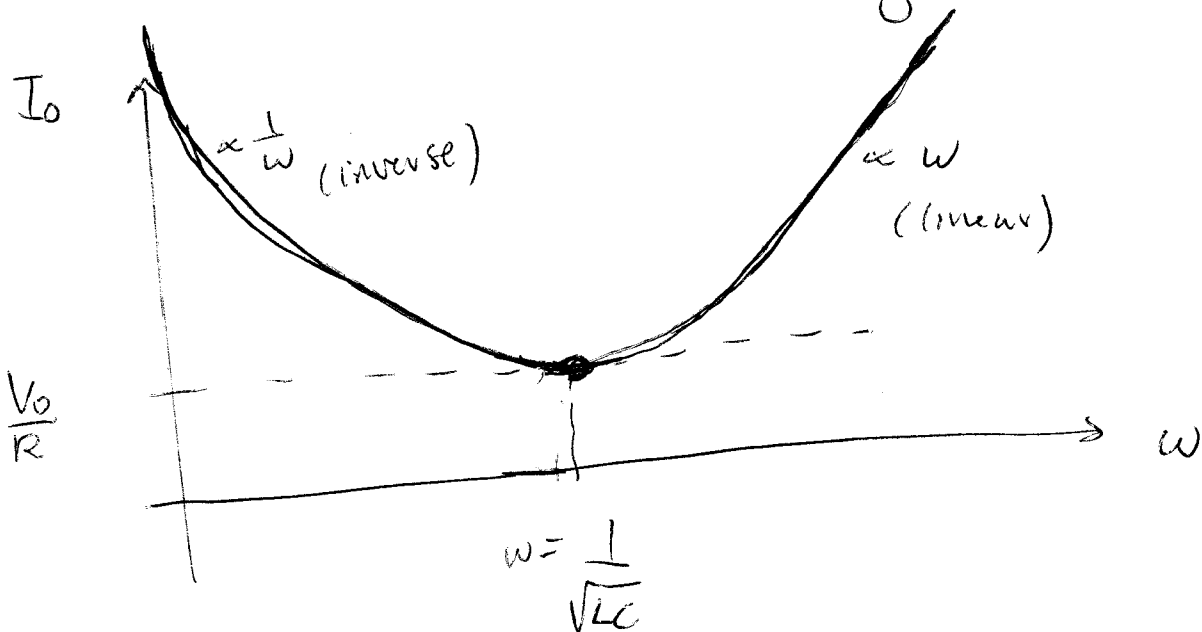
(c) For values of $\omega \ll 1/\sqrt{LC}$, show that I_0 can be approximated as $I_0 \approx B\omega^m$. Determine B and m . (2 marks)

for $\omega \rightarrow 0$ $I_0 \approx V_0 \sqrt{\frac{1}{R^2} + \left(-\frac{1}{\omega L}\right)^2} \approx \frac{V_0}{\omega L}$
 $\therefore B = \frac{V_0}{L}$
 $m = -1$

a plot

(c) Sketch plots of I_0 versus ω and ϕ versus ω . On your plots, label the points where $\omega = 1/\sqrt{LC}$. (4 marks)

when $\omega = \frac{1}{\sqrt{LC}}$ $I_0 = V_0 \sqrt{\frac{1}{R^2} + \left(\frac{C}{\sqrt{LC}} - \frac{\sqrt{LC}}{L}\right)^2}$
 $= V_0 \sqrt{\frac{1}{R^2} + \left(\frac{\sqrt{C}}{\sqrt{L}} - \frac{\sqrt{C}}{\sqrt{L}}\right)^2} = \frac{V_0}{R}$



(10pts) 5. Make use of Euler's equation ($e^{\pm j\phi} = \cos \phi \pm j \sin \phi$) to help you evaluate the following integral:

$$\int_0^{\pi/4} e^x \cos x dx$$

You must show all of your work to receive full credit.

$$\left. \begin{aligned} e^{jx} &= \cos x + j \sin x \\ e^{-jx} &= \cos x - j \sin x \end{aligned} \right\} \text{add these two}$$

$$e^{jx} + e^{-jx} = 2 \cos x \quad \Rightarrow \cos x = \frac{1}{2}(e^{jx} + e^{-jx})$$

difference gives $\sin x = \frac{1}{2j}(e^{jx} - e^{-jx})$

$$\int_0^{\pi/4} e^x \cos x dx = \int_0^{\pi/4} e^x \frac{(e^{jx} + e^{-jx})}{2} dx = \frac{1}{2} \int_0^{\pi/4} (e^{(1+j)x} + e^{(1-j)x}) dx$$

$$= \frac{1}{2} \left[\frac{1}{1+j} e^{(1+j)x} + \frac{1}{1-j} e^{(1-j)x} \right] \Big|_0^{\pi/4}$$

$$= \frac{1}{2} \left[\frac{e^x e^{jx}}{1+j} + \frac{e^x e^{-jx}}{1-j} \right] \Big|_0^{\pi/4} = \frac{1}{2} \left(\frac{1-j}{2} e^x e^{jx} + \frac{1+j}{2} e^x e^{-jx} \right) \Big|_0^{\pi/4}$$

$$= \frac{1}{4} \left[(e^x e^{jx} + e^x e^{-jx}) - j(e^x e^{jx} - e^x e^{-jx}) \right] \Big|_0^{\pi/4}$$

$$= \frac{1}{2} \left[e^x \left(\frac{e^{jx} + e^{-jx}}{2} \right) + e^x \left(\frac{e^{jx} - e^{-jx}}{2j} \right) \right] \Big|_0^{\pi/4}$$

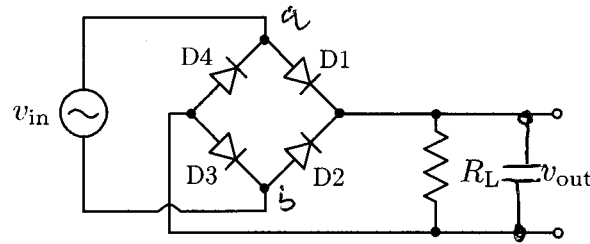
$$= \frac{e^x}{2} (\cos x + \sin x) \Big|_0^{\pi/4}$$

$$= \frac{e^{\pi/4}}{2} \left(\cos \frac{\pi}{4} + \sin \frac{\pi}{4} \right) - \frac{e^0}{2} (\cos 0 + \sin 0)$$

$$\therefore \int_0^{\pi/4} e^x \cos x \, dx = \frac{e^{\pi/4}}{2} \frac{2}{\sqrt{2}} - \frac{1}{2}$$

$$= \frac{e^{\pi/4}}{\sqrt{2}} - \frac{1}{2} = 1.0509$$

(10pts) 6. The circuit below consists of a sinusoidal input v_{in} , four diodes, and a resistor R_L . The output of the circuit v_{out} is taken to be the voltage across R_L .



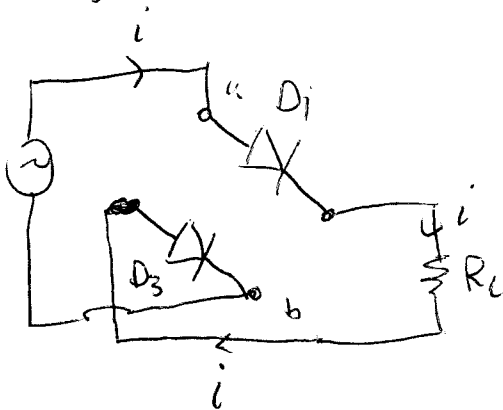
(a) The next page shows a plot of v_{in} versus time. On the axes directly below, sketch a plot of v_{out} versus time. Draw your plot to scale as best you can. (7 marks)

(b) With the addition of a single capacitor C , this circuit can be made into an AC-to-DC converter. Add the required capacitor to the circuit above. How should the product $R_L C$ compare to the period T of the AC input v_{in} in order for the circuit to work as an effective AC-to-DC converter? (3 marks)

(b) want the capacitor discharge time to be slow.
 \therefore require $R_L C \gg T$.

(a) assume v_{in} is in positive part of cycle. \rightarrow a positive w.r.t. b

D_1 forward biased
 D_3 forward biased.



$$v_{in} - V_{D1} - \underbrace{iR_L}_{V_{out}} - V_{D3} = 0$$

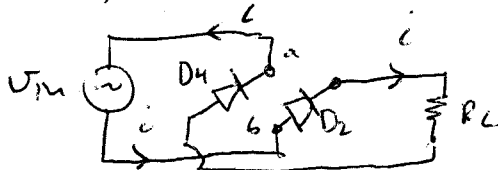
$$V_{out} = iR_L$$

$$\therefore V_{out} = v_{in} - V_{D1} - V_{D3} = v_{in} - 2V_D$$

where $V_D \approx 0.6V$
 for forward biased diode.

when v_{in} is in neg. part of cycle \rightarrow b positive. w.r.t. a

D_2, D_4 forward biased.



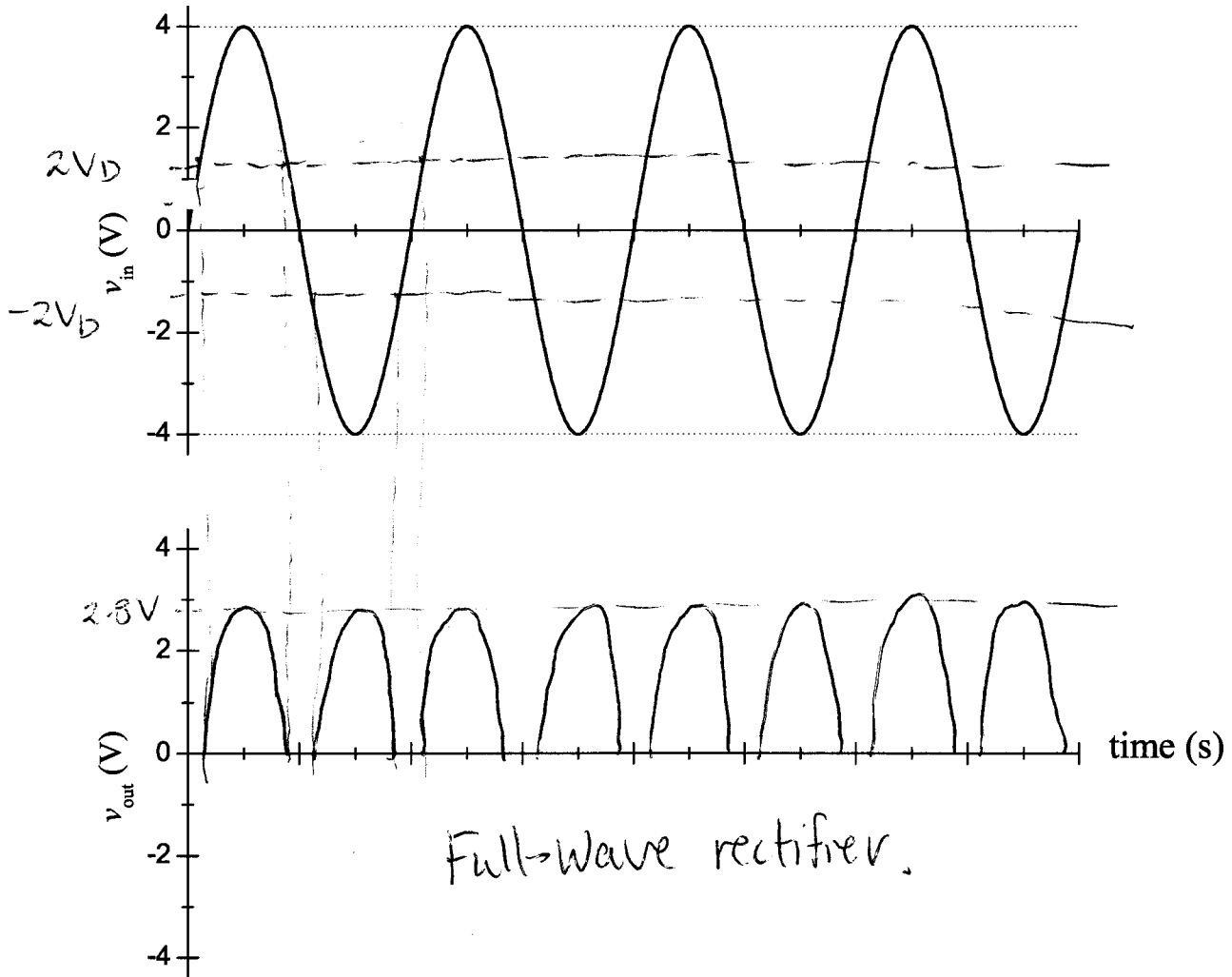
$$V_{out} = +iR_L$$

$$-v_{in} - V_{D2} - iR_L - V_{D4} = 0$$

$$\therefore V_{out} = -v_{in} - 2V_D$$

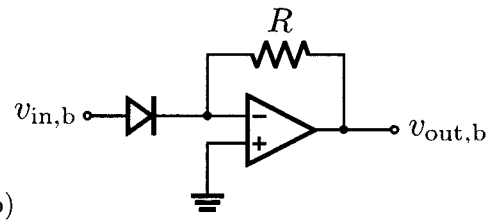
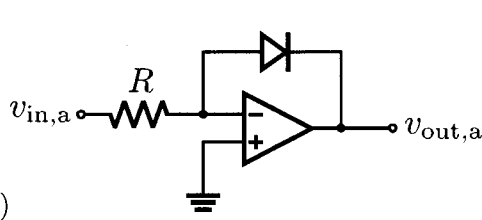
10 pts

$$4V - 2V_D \approx 4V - 1.2V = 2.8V$$



Full-Wave rectifier.

(10pts) 7. Figures (a) and (b) below show the log- and the anti-log-amplifiers respectively.



(a)

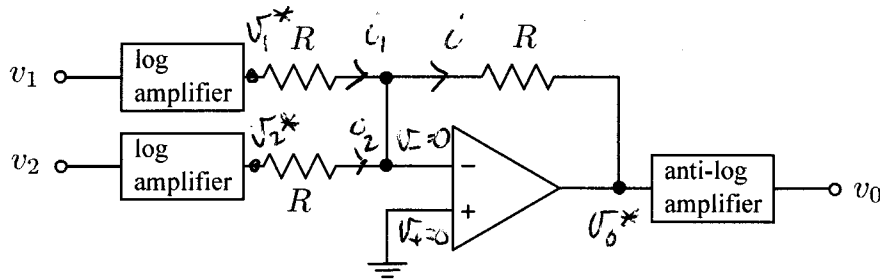
(b)

The outputs of the circuits are given by:

$$v_{out,a} = -\frac{k_B T}{e} \ln \frac{v_{in,a}}{I_0 R}$$

$$v_{out,b} = -I_0 R \exp\left(\frac{e v_{in,b}}{k_B T}\right)$$

The circuit below makes use of the log and anti-log amplifiers. In this circuit the box labelled "log amplifier" corresponds to circuit (a) above and the box labelled "anti-log amplifier" corresponds to circuit (b) above. Assume that all resistors used in this problem are identical and that all diodes used in this problem are identical.



Find an expression for v_0 of this circuit. What kind of function does this circuit perform?

$$U_1^* - U_1 R = U_- = 0 \quad \therefore U_1 = \frac{U_1^*}{R} \quad \text{likewise } U_2 = \frac{U_2^*}{R}$$

$$i = U_1 + U_2 = \frac{U_1^* + U_2^*}{R}$$

$$U_- - iR = U_0^* \quad \therefore U_0^* = -\left(\frac{U_1^* + U_2^*}{R}\right)R = -(U_1^* + U_2^*)$$

$$U_1^* = -\frac{k_B T}{e} \ln\left(\frac{U_1}{I_0 R}\right) \quad U_2^* = -\frac{k_B T}{e} \ln\left(\frac{U_2}{I_0 R}\right)$$

$$\therefore U_0^* = \frac{k_B T}{e} \left[\ln \frac{U_1}{I_0 R} + \ln \frac{U_2}{I_0 R} \right] = \frac{k_B T}{e} \ln \left(\frac{U_1 U_2}{(I_0 R)^2} \right)$$

10 pts

$$V_0 = -I_0 R \exp\left[\frac{e V_0}{k_B T}\right]$$

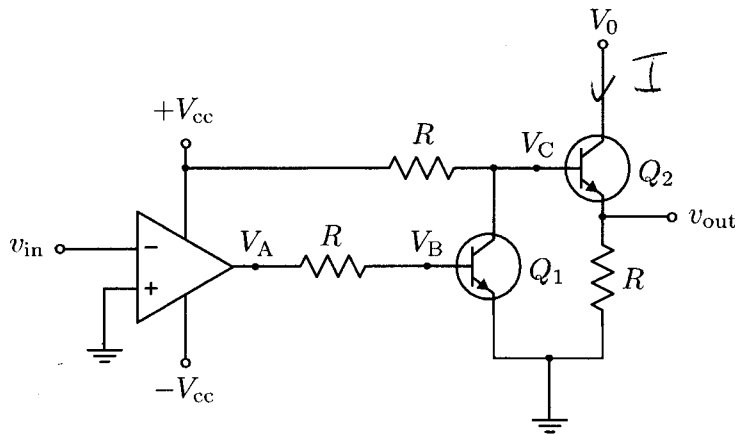
$$= -I_0 R \exp\left[\frac{e}{k_B T} \frac{k_B T}{e} \ln\left(\frac{V_1 V_2}{(I_0 R)^2}\right)\right]$$

$$= -I_0 R \frac{V_1 V_2}{(I_0 R)^2}$$

$$\therefore V_0 = - \frac{V_1 V_2}{I_0 R}$$

This circuit takes the product of V_1 & V_2 .

(10pts) 8. The circuit shown below is similar (but not identical) to a circuit that you built and studied in Experiment #6.



Assume that $R = 10\text{ k}\Omega$, $V_{cc} = 15\text{ V}$, and $V_0 = 5\text{ V}$. In this problem you are simply asked to complete the table shown below. For the input voltages v_{in} shown in the table, enter the resulting values for V_A , V_B , V_C , and v_{out} . In the Q_1 and Q_2 columns indicate whether each transistor is conducting or not conducting. If a transistor is in its conducting state, enter "ON". If a transistor is not conducting, enter "OFF".

v_{in} (V)	V_A (V)	V_B (V)	V_C (V)	Q_1	Q_2	v_{out} (V)
-3	+15V	+15V	0	ON	OFF	0
-1	+15V	+15V	0	ON	OFF	0
+1	-15V	-15V	+15V	OFF	ON	+5V
+5	-15V	-15V	+15V	OFF	ON	+5V

$V_A = A_{OL}(V_+ - V_-) = -A_{OL}V_-$ where A_{OL} large.

\therefore if $V_- < 0$, $V_A \rightarrow +V_{cc}$

$V_- > 0$, $V_A \rightarrow -V_{cc}$

current into base of transistor very small. $\therefore V_A \approx V_B$

If voltage at transistor base exceeds the emitter voltage by about 0.6 V it is conducting (ON). Otherwise it is OFF

If Q_1 is conducting $V_C \approx 0$. If Q_1 OFF $V_C \approx V_{cc}$

If Q_2 conducting $V_{out} \approx IR \approx V_0$. If Q_2 OFF $V_{out} \approx IR = 0$ since $I \approx 0$

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